



Recent Developments in Understanding the Fatigue Behavior of PEEK Materials

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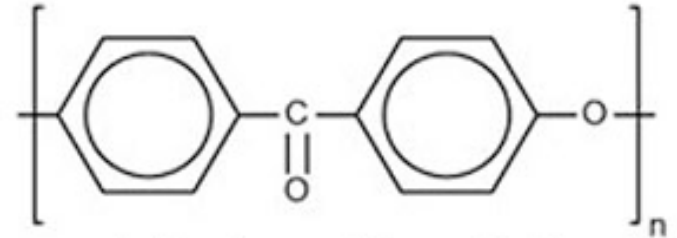
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PEEK as a substitute for metallic alloys in orthopaedic applications



General properties/characteristics:

- A high performance engineering thermoplastic – good mechanical and wear properties - can be molded into complex shapes - can be reinforced
- Ultimate Stress ~ 100MPa; Elastic modulus about 3 GPa
- T_g ~ 143C
- Semi-crystalline, ~30%-35%
- Resistant to high ionizing radiation and chemical attack
- Stable up to 300C
- Biocompatible; biologically inert

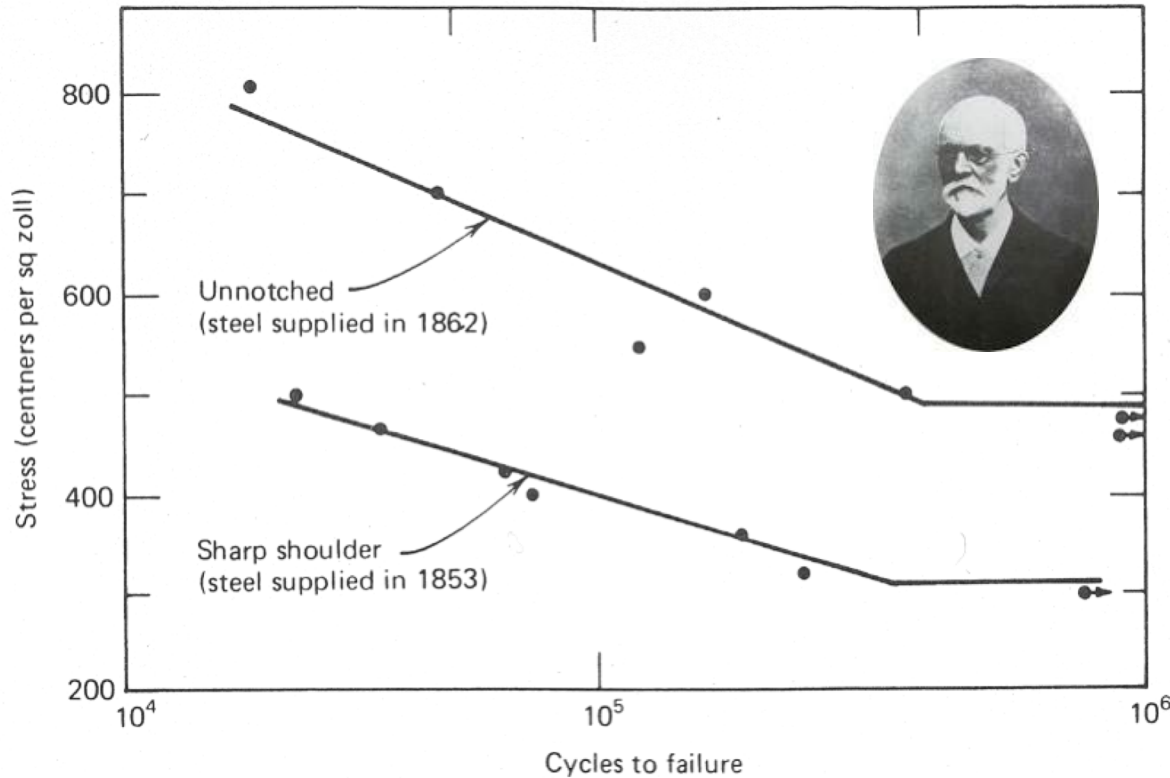
PEEK as a substitute for metallic alloys in medical device applications – mechanical considerations

- Are the mechanical properties (deformation, creep, fracture, fatigue) adequate for load-bearing musculoskeletal applications?
- **Focus of this overview** – recent studies characterizing the fatigue resistance of PEEK and PEEK composites

Brief background - Three approaches to fatigue analyses:

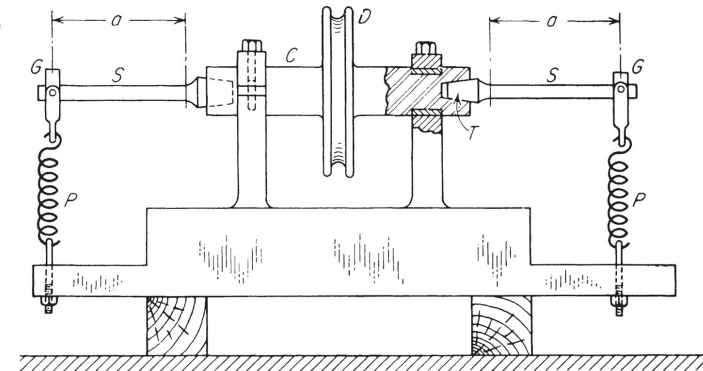
- Stress-Life (S-N)
- Strain-Life (ϵ -N)
- Fracture mechanics

S-N Fatigue Approach (The Wöhler Curve)

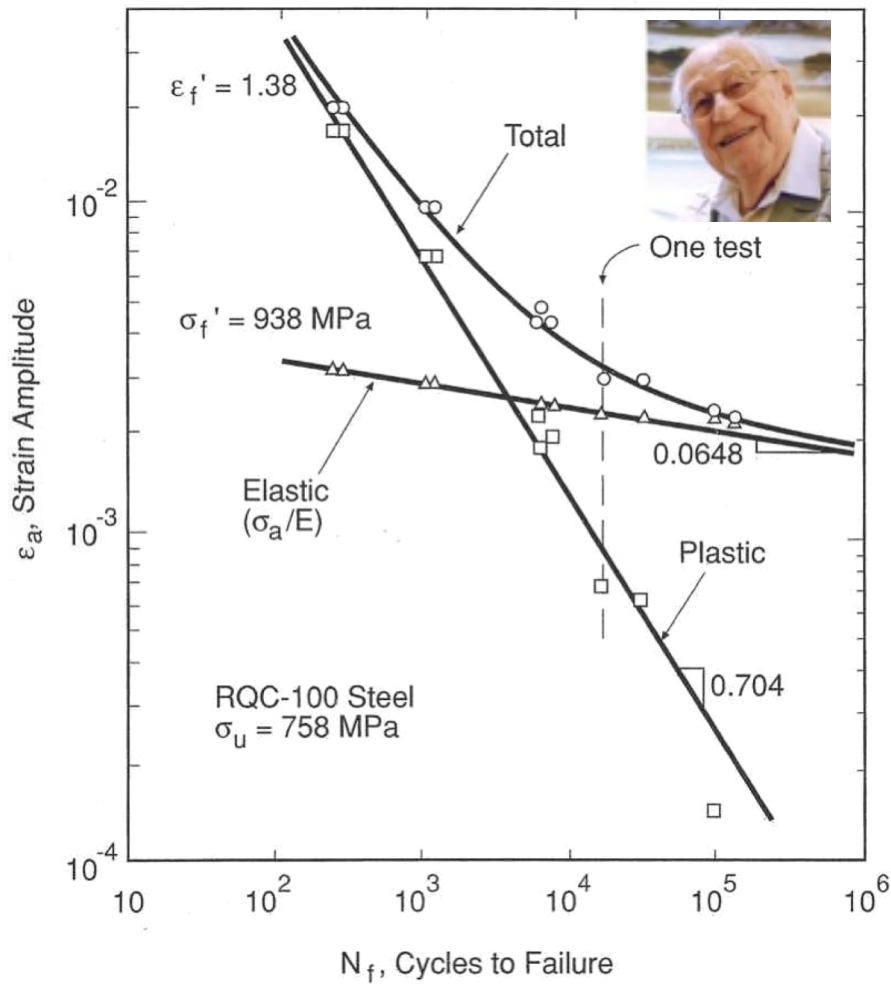


A total life approach:
 $N_i + N_p = N_f$

Most useful when plastic strains are small
(high-cycle fatigue)



ϵ -N Fatigue Approach (Manson-Coffin)



Also a total life approach:

$$N_i + N_p = N_f$$

$$\epsilon_a = (\sigma_f'/E)(2N_f)^b + \epsilon_f'(2N_f)^c$$

$$\epsilon_a = \sigma_a/E + (\sigma_a/K')^{1/n'}$$

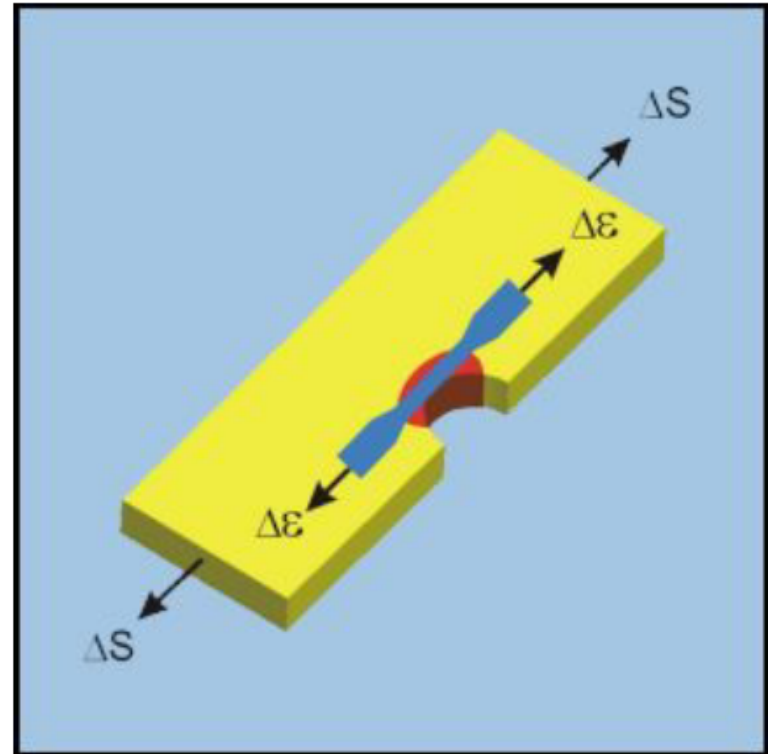
Can accommodate large plastic strains

(low- and high-cycle fatigue regimes)

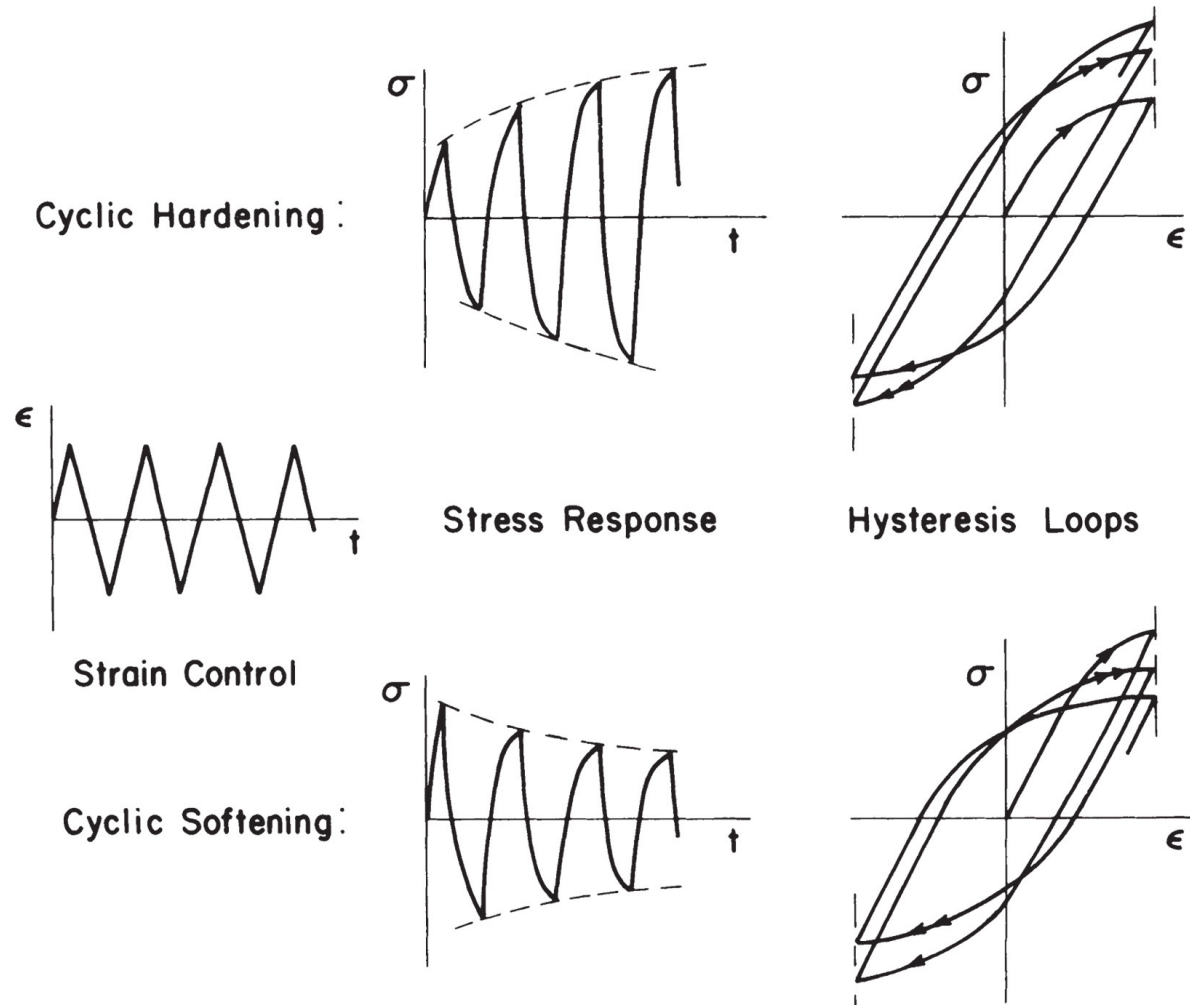


ϵ -N Fatigue Approach

- This approach considers Plastic deformation such as might occur locally at a notch
- That is, *regardless of the external mode of loading* (cyclic stress or strain controlled), the *notch experiences a strain-controlled condition* due to the surrounding mass of elastic material

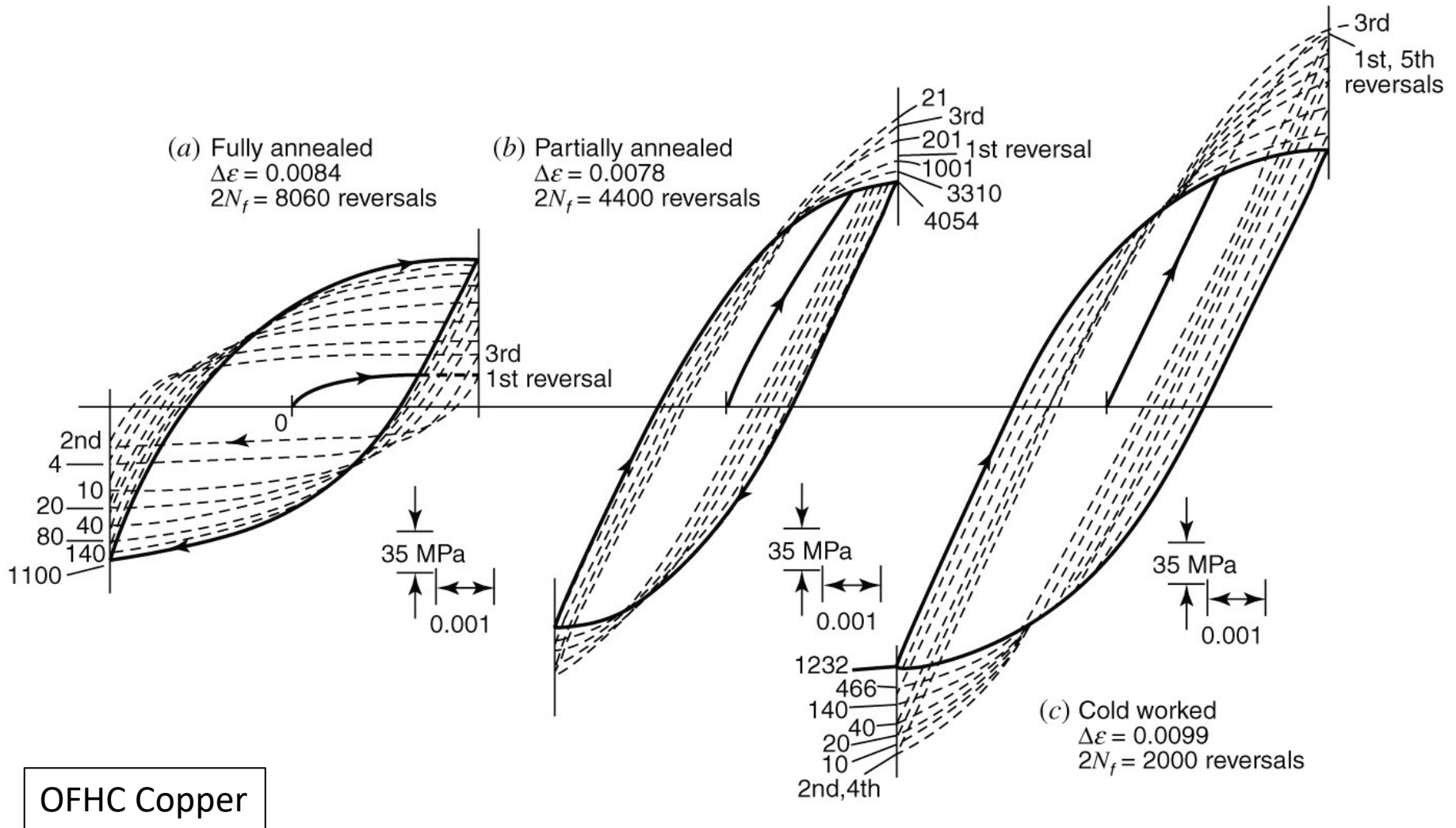


Cyclic Hardening/Softening seen in ϵ -N Tests

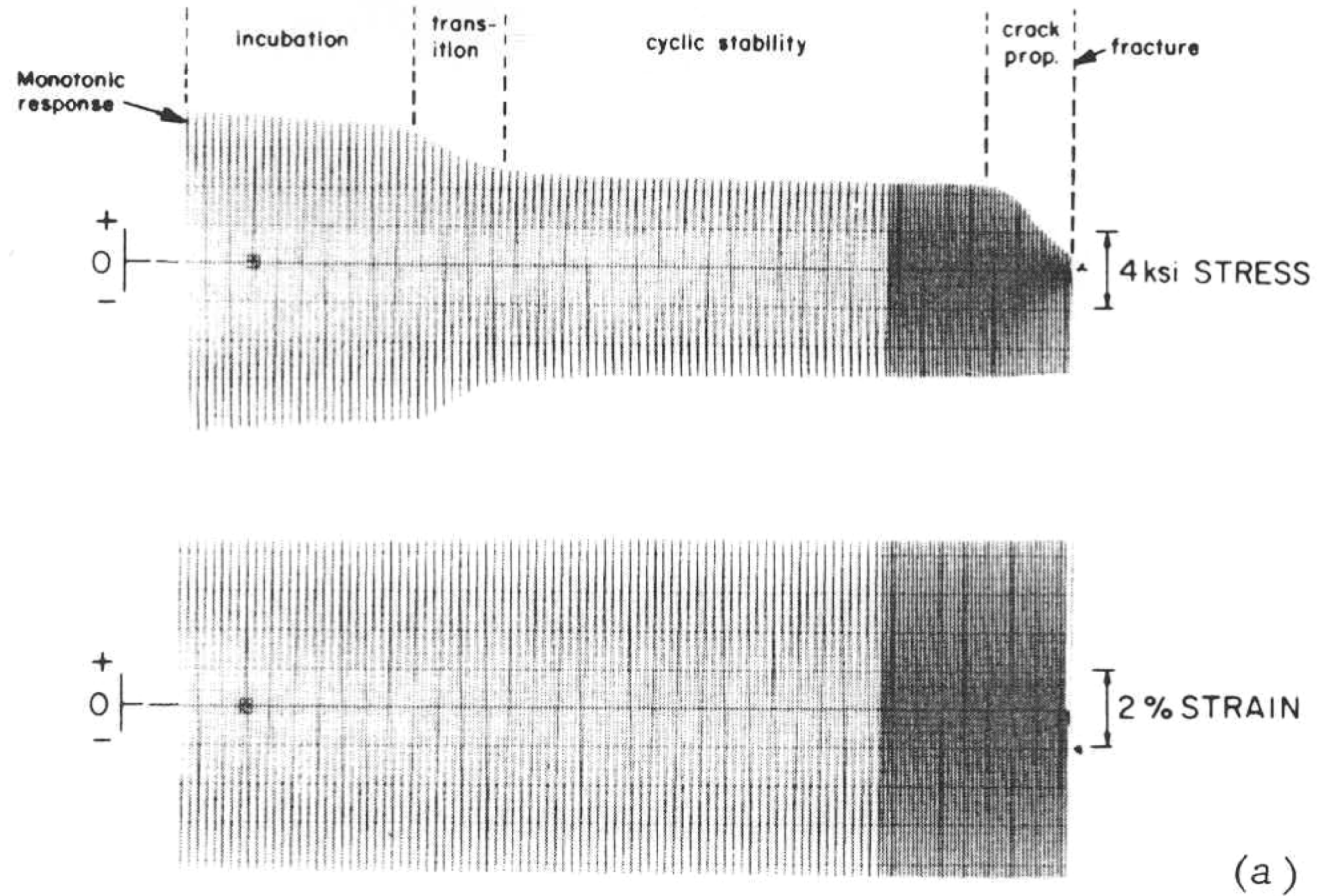


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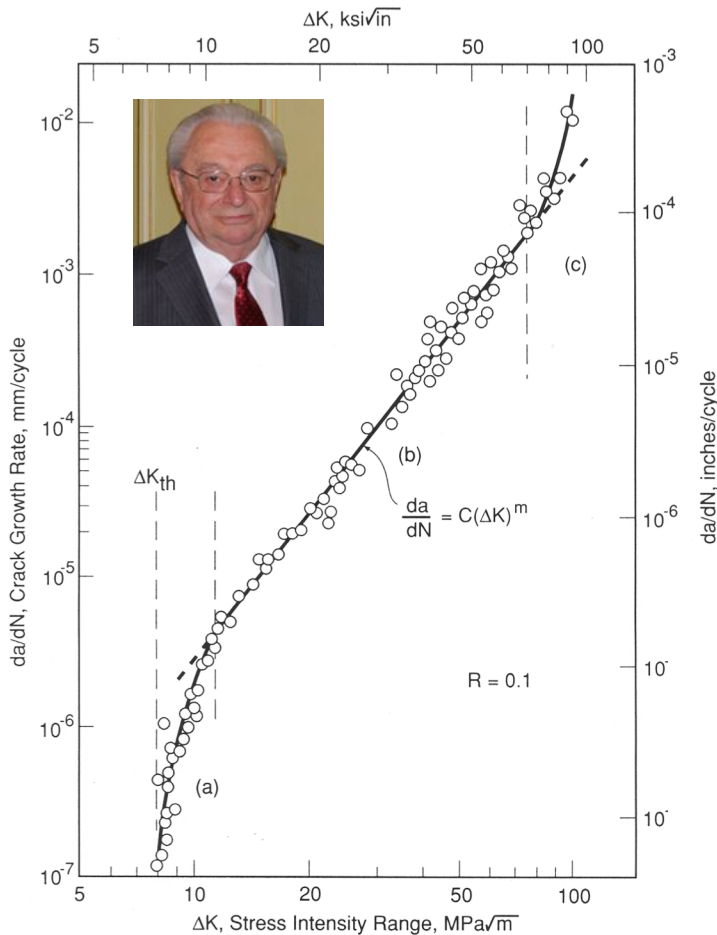
Metals can Cyclic Harden or Soften



Polymers only Cyclically Soften



Fatigue Crack Propagation Approach (Paris law)

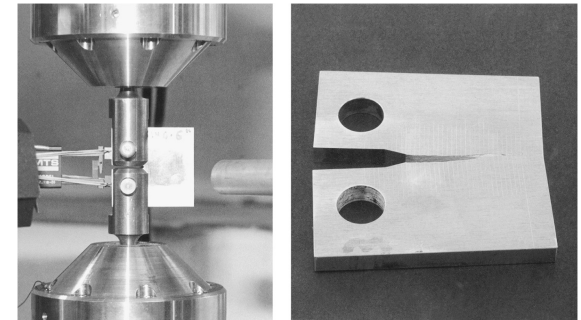
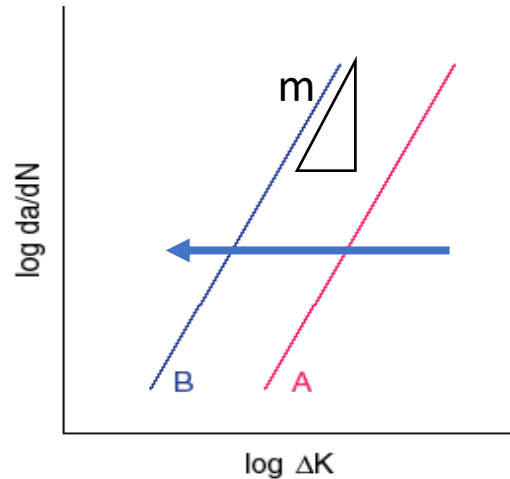


Focus is on the *kinetics* of fatigue crack growth (N_p)

$$\frac{da}{dN} = C\Delta K^m$$

$$\Delta K = \Delta\sigma(F)(\pi a)^{0.5}$$

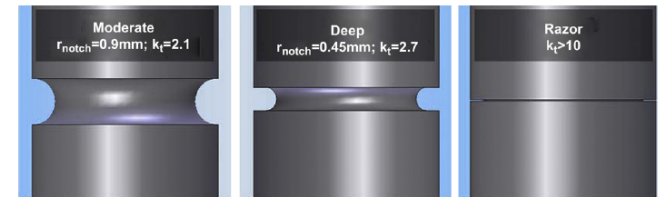
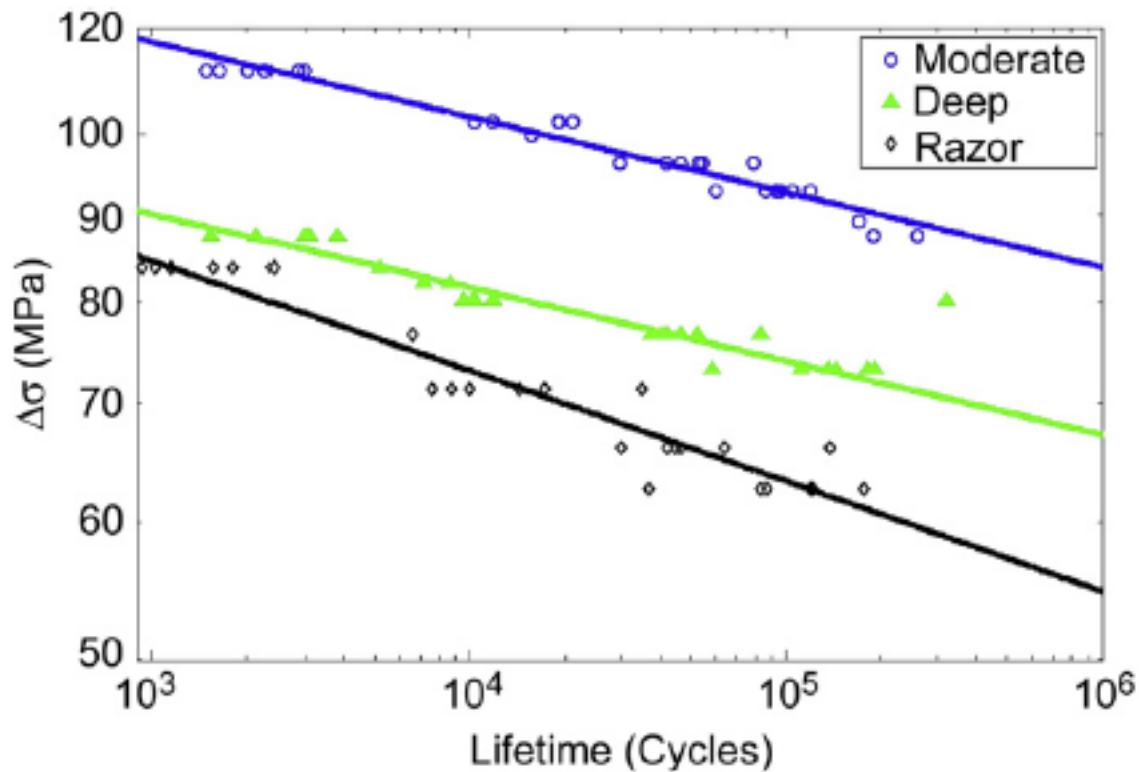
where da/dN = fatigue crack growth rate;
 ΔK = stress intensity factor range; and,
 $C, m = f(\text{material variables, environment, frequency, temperature, stress ratio})$
 C is the intercept at $\Delta K = 1$; m is the slope



Fatigue Behavior of PEEK Materials

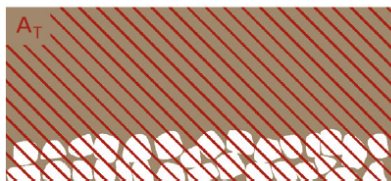
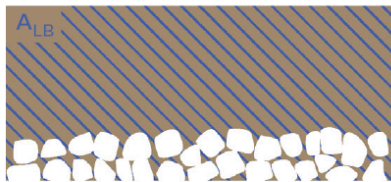
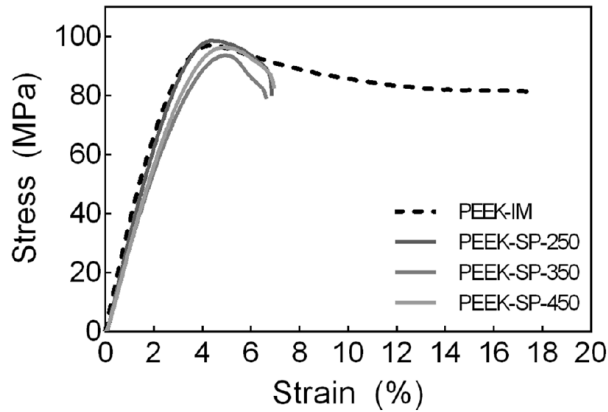
Recent Studies

S-N Fatigue of PEEK is Notch Sensitive

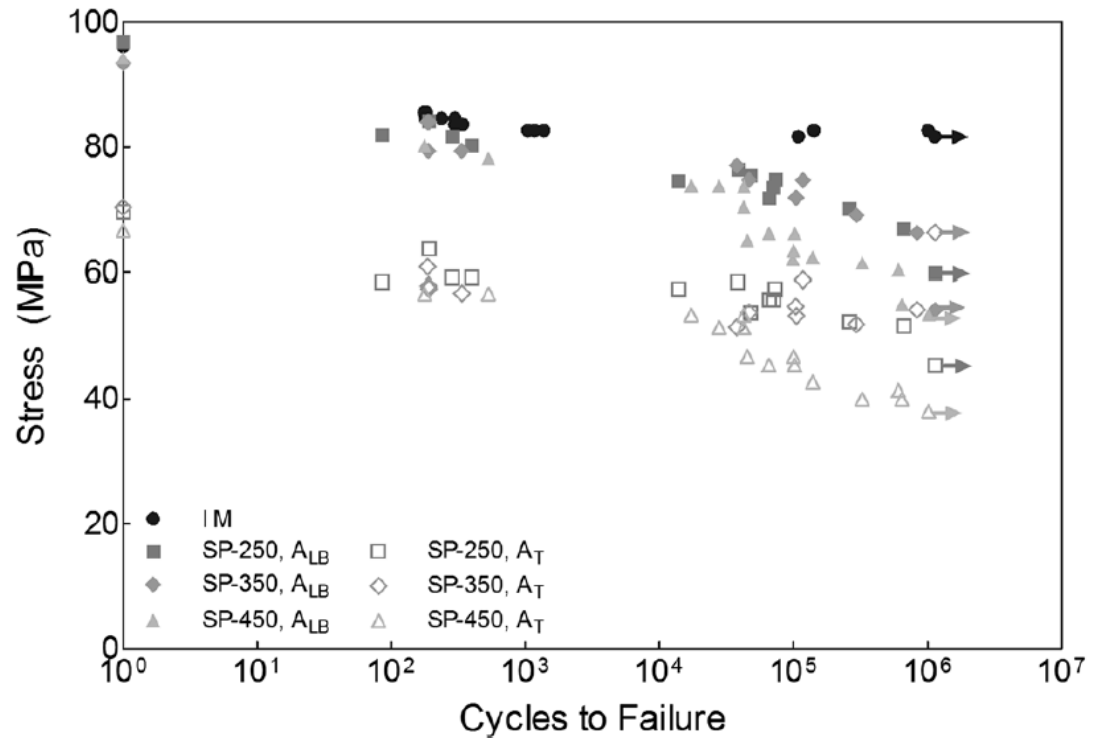


- N_i shortened with increase in notch severity
- Optima LT1, Invibio; $R \sim 0$; Preconditioned and tested in 37C PBS solution; 2 Hz

S-N Fatigue of PEEK is Notch Sensitive

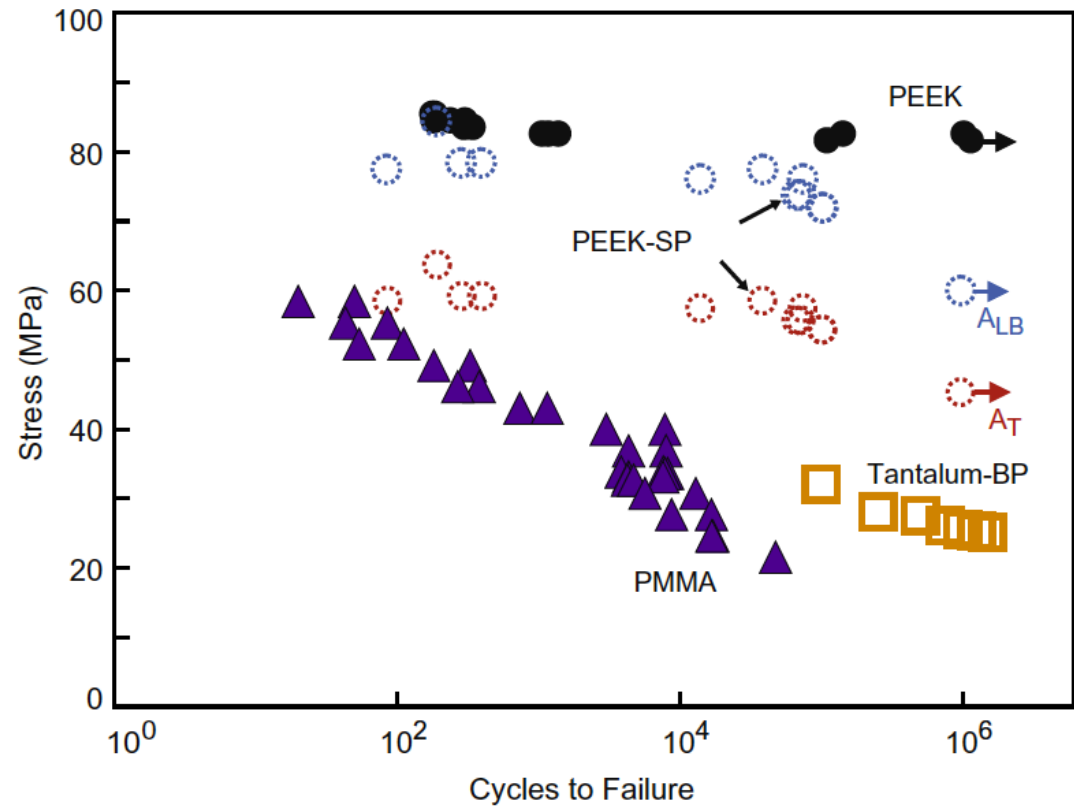
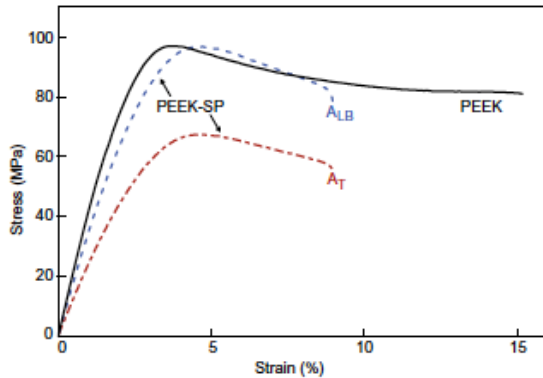


$$A_T = A_{LB} + A_{PORE}$$



- Again, very high cyclic stresses required for failure of IM PEEK
- Surface porosity negatively affects S-N fatigue life
- Zeniva™ 500, Solvay Specialty Polymers; R = 0.05; RT; 1 Hz

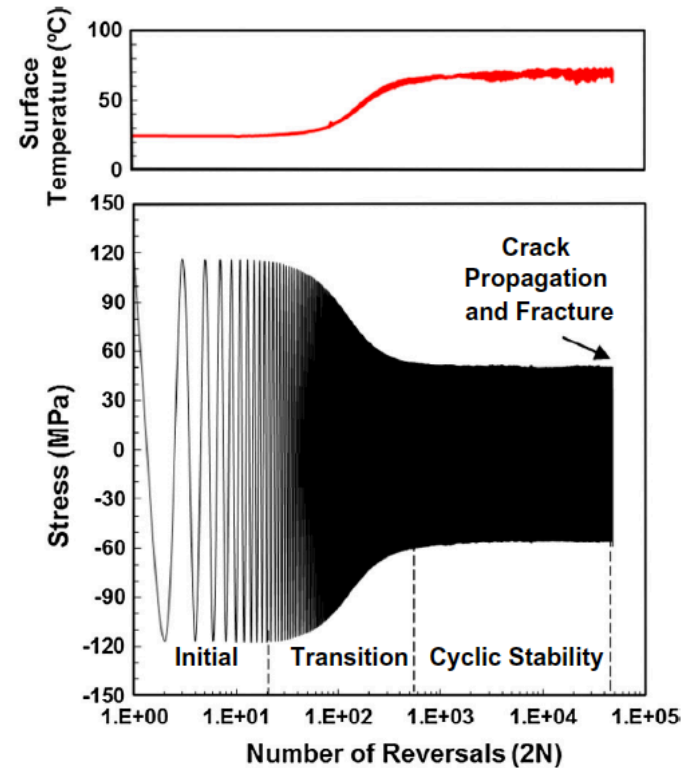
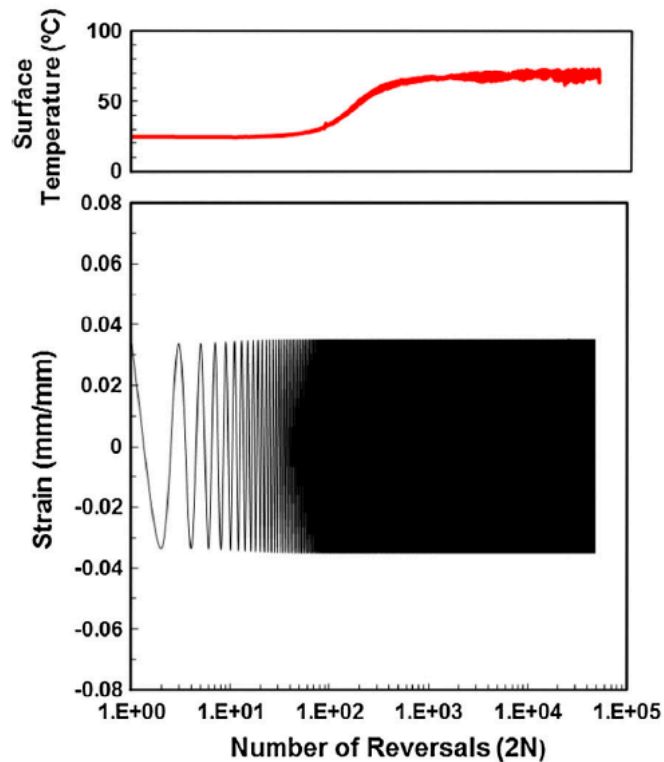
Surface porous PEEK S-N Fatigue Compares Favorably with PMMA and Porous Tantalum



S-N Fatigue of PEEK - Observations

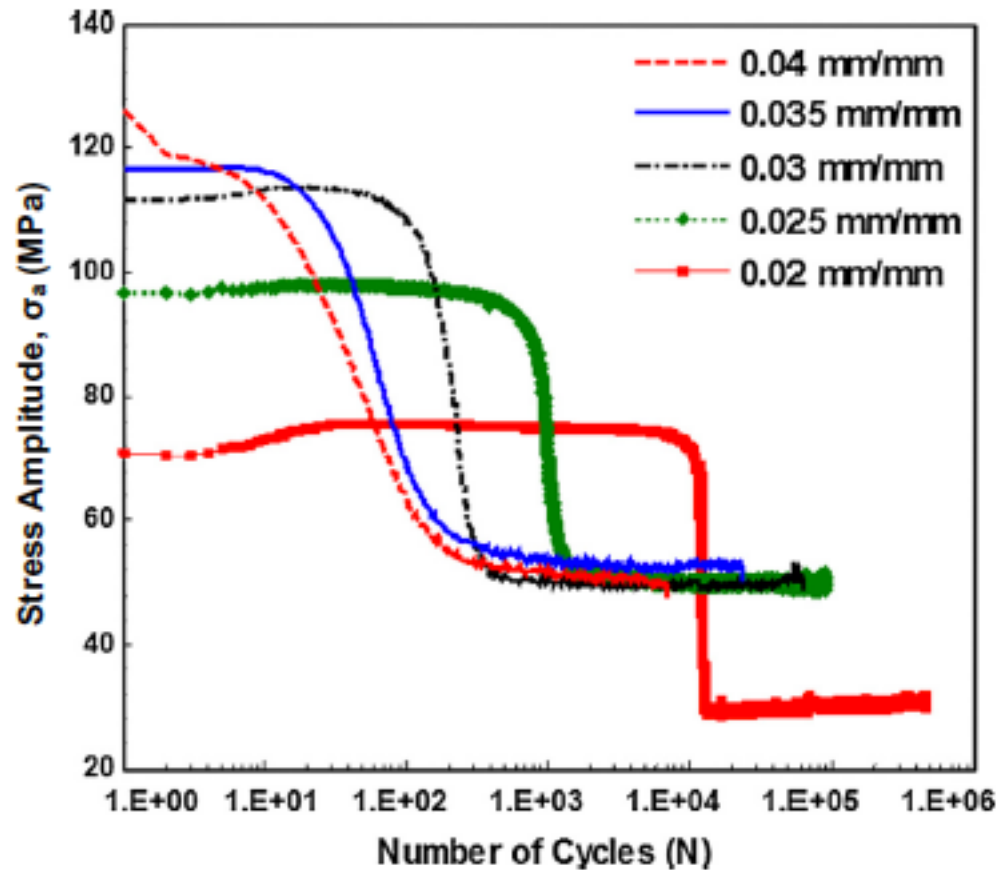
- Unfilled PEEK demonstrates quite good S-N fatigue behavior, at RT and PBS 37C
- Maintains reasonable S-N life with surface porosity
- Notching and severe stress concentrations will reduce life via truncation of N_i

ϵ -N Fatigue of PEEK



- PEEK exhibits cyclic softening, consistent with other polymers
- Note the surface temperature rise to 50-60C ($T_g = 143C$); there appears to be a thermal component contribution in these tests (reduction in elastic modulus)
- The presence of a transition is consistent with other thermoplastic polymers
- TECA PEEK™, Ensinger; R= -1 (strain); RT; 0.5 Hz

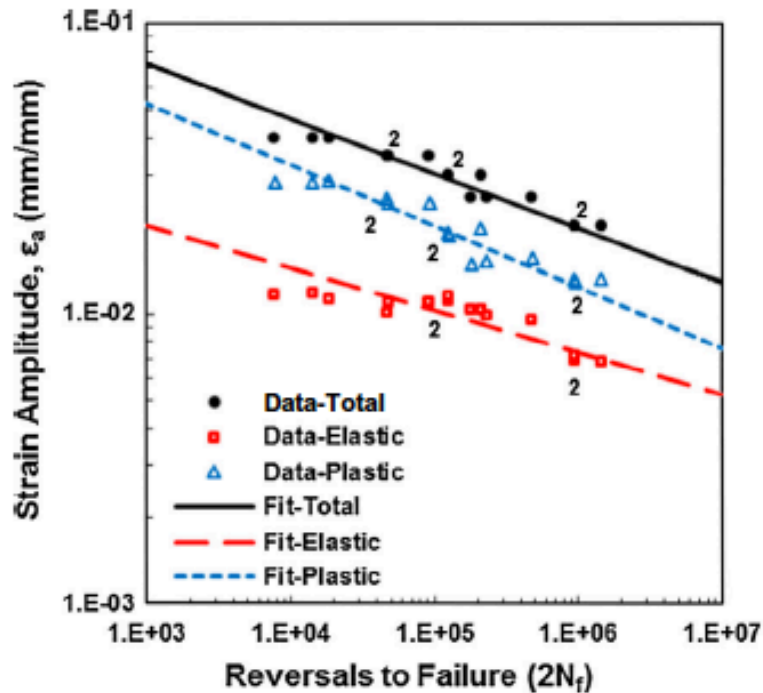
ϵ -N Fatigue of PEEK



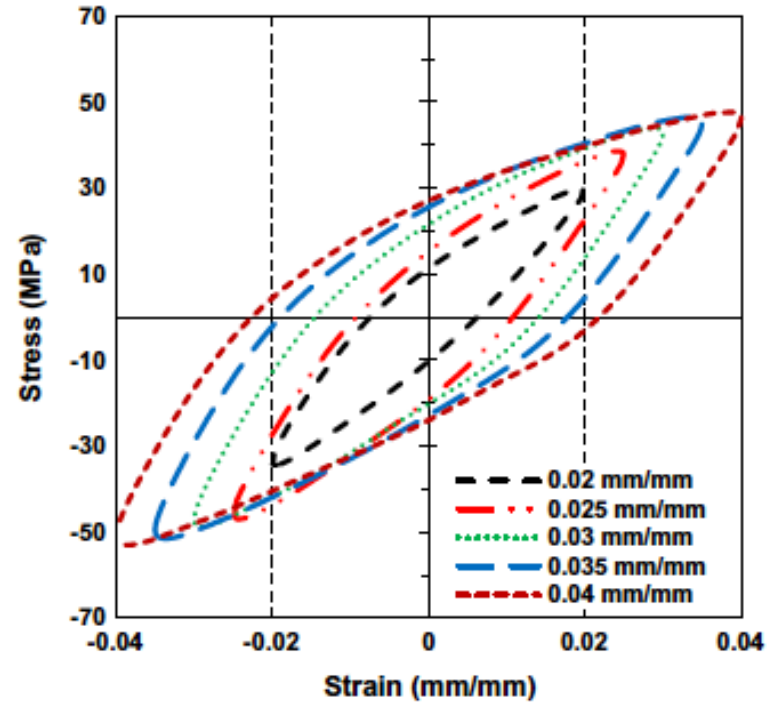
Cyclic softening occurs more rapidly at higher strain rates

At all strain rates, there is an initial phase, followed by transition, followed by steady-state

ϵ -N Fatigue of PEEK



(a)



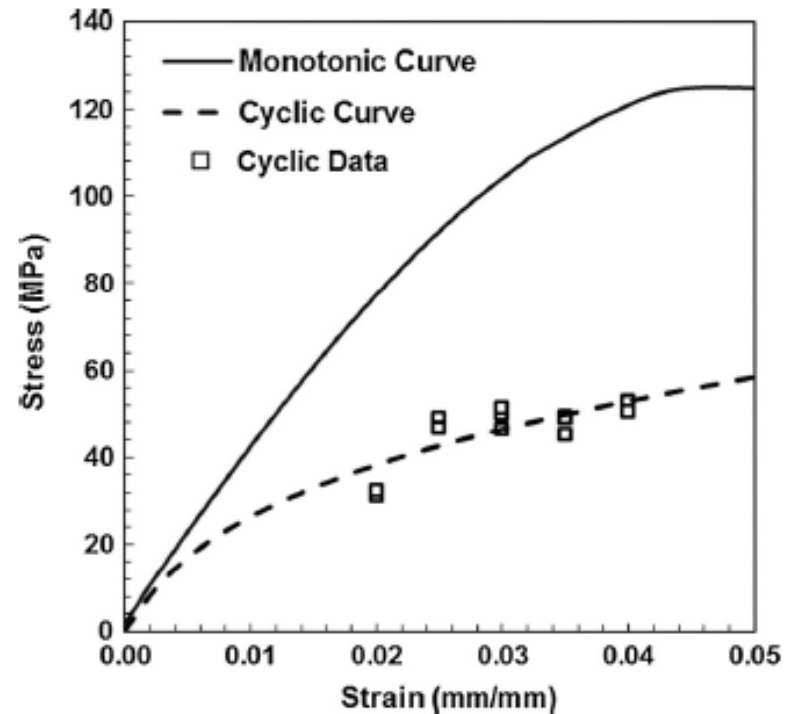
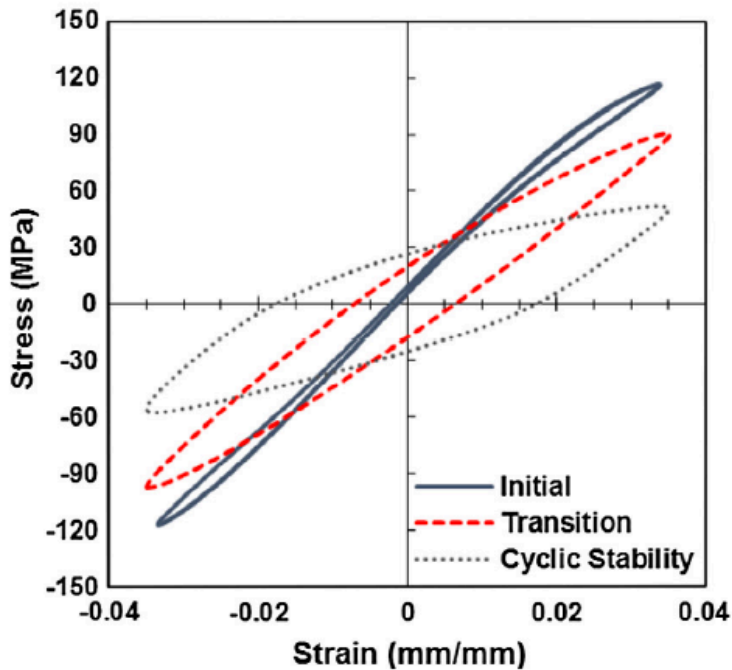
(b)

ϵ -N life can be decomposed into elastic and plastic strains per Manson-Coffin relationship

Plastic strains dominate, even in the high cycle fatigue regime

$$\epsilon_a = (\sigma'_f/E)(2N_f)^b + \epsilon'_f(2N_f)^c$$

ϵ -N Fatigue of PEEK



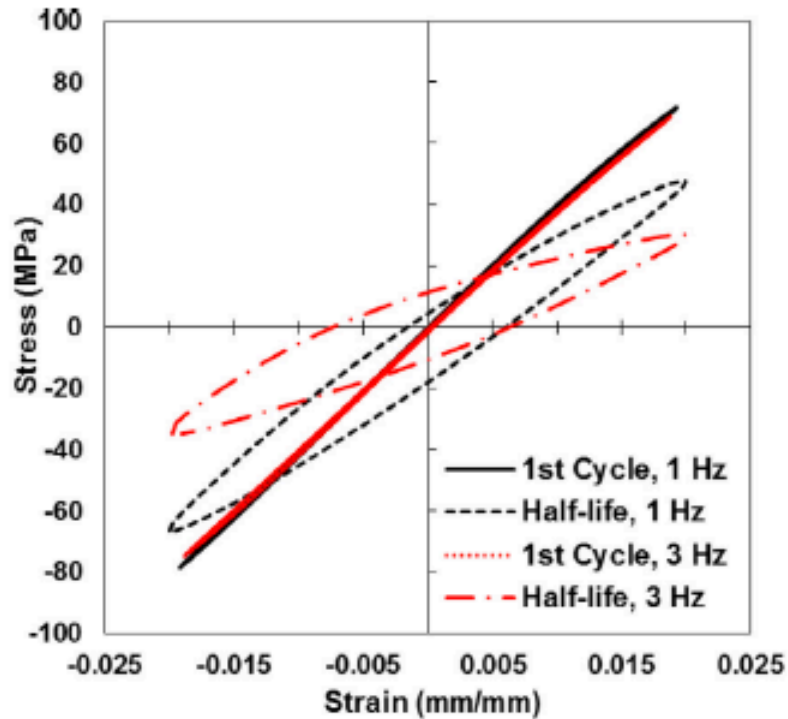
- With softening, the hysteresis loop is enlarged
- A cyclically-stabilized σ - ϵ curve can be compared to the monotonic
- Model using a Ramberg-Osgood approach: $\epsilon_e = \sigma/E$ $\epsilon_p = (\sigma/K')^{1/n'}$

$$(\epsilon_p \rightarrow \sigma = K' \epsilon_p^{n'})$$

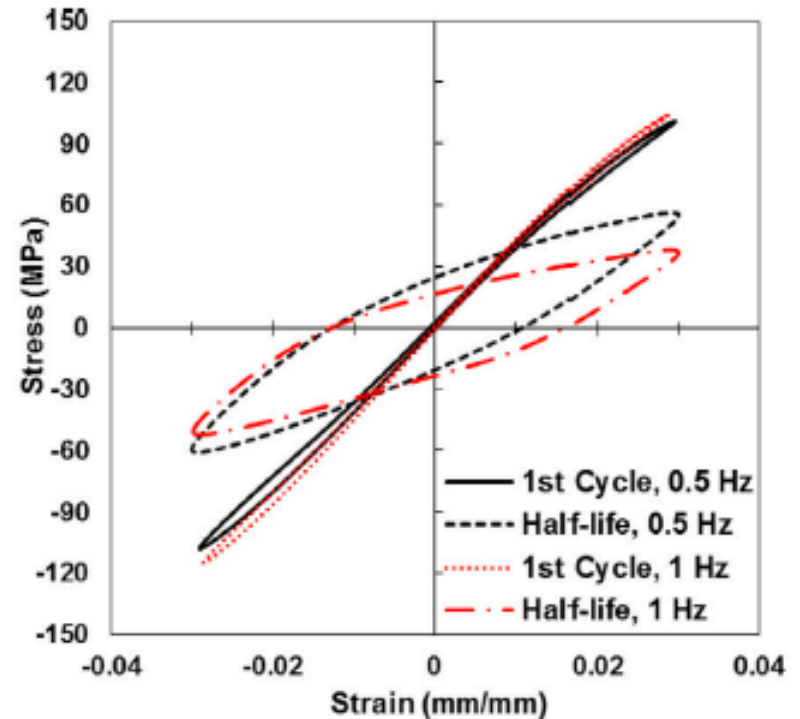
Where K' is the cycle strength coefficient and n' is the cyclic strain hardening exponent

$$\epsilon_a = \epsilon_e + \epsilon_p$$

ϵ -N Fatigue of PEEK



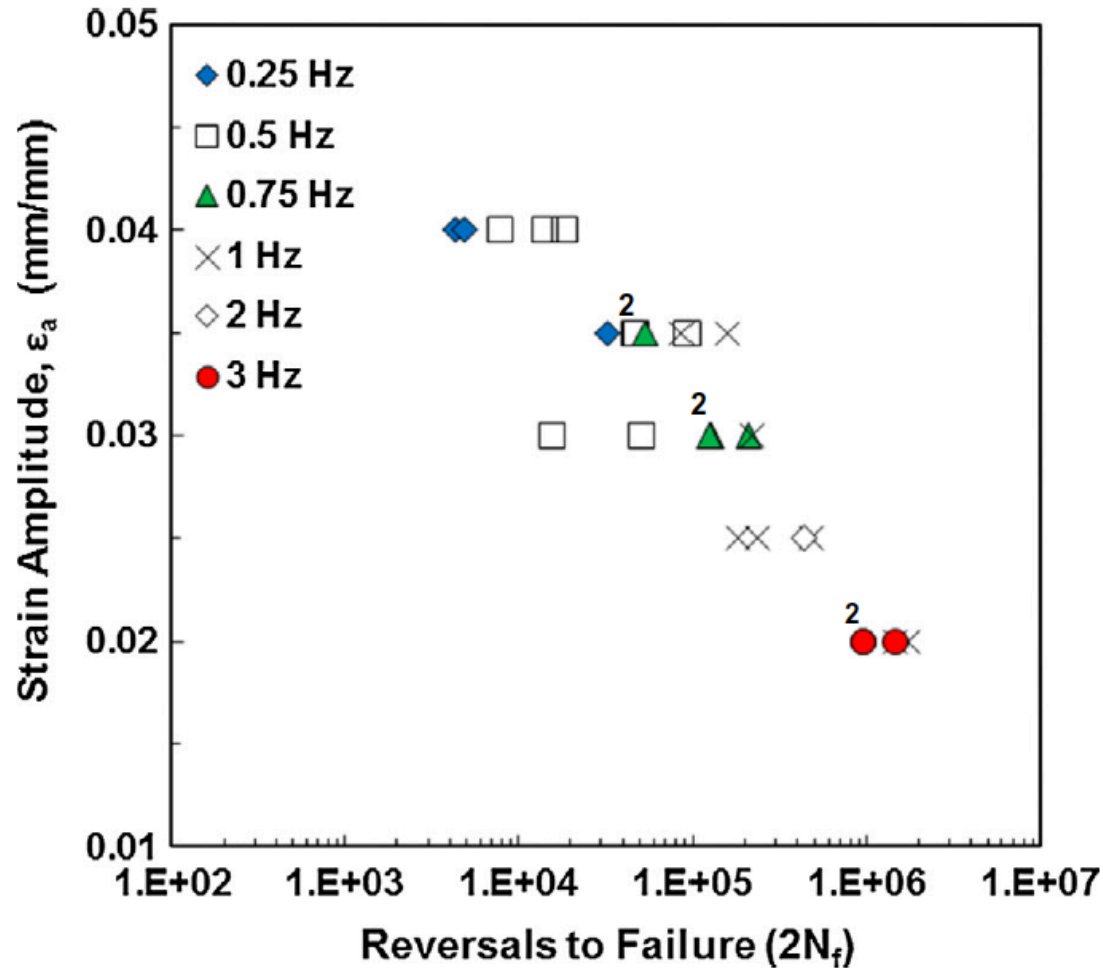
(a)



(a)

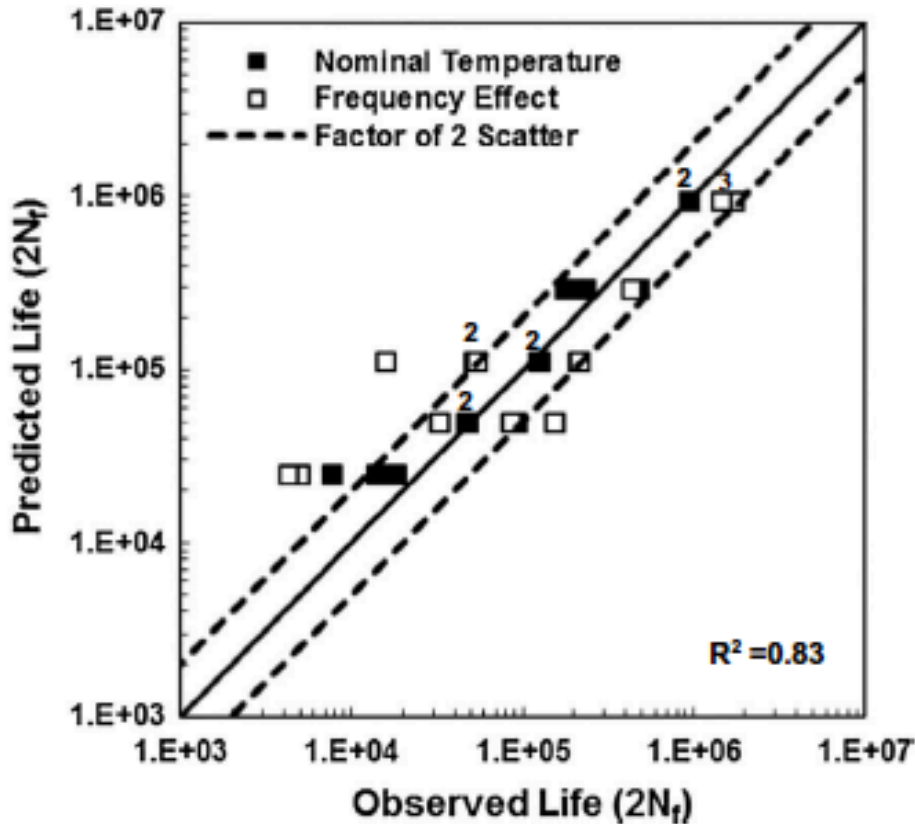
- Cyclic behavior is affected by test frequency
- Note the hysteresis expansion with increase in test frequency
- Specimen temperature increased somewhat with increase in test frequency
- Degradation in modulus was observed

ϵ -N Fatigue of PEEK



- Cyclic lifetime may increase with an increase in test frequency

ϵ -N Fatigue of PEEK



ϵ -N N_f can be reasonably predicted using the Manson-Coffin relationship

ϵ -N Fatigue of PEEK – crack initiation

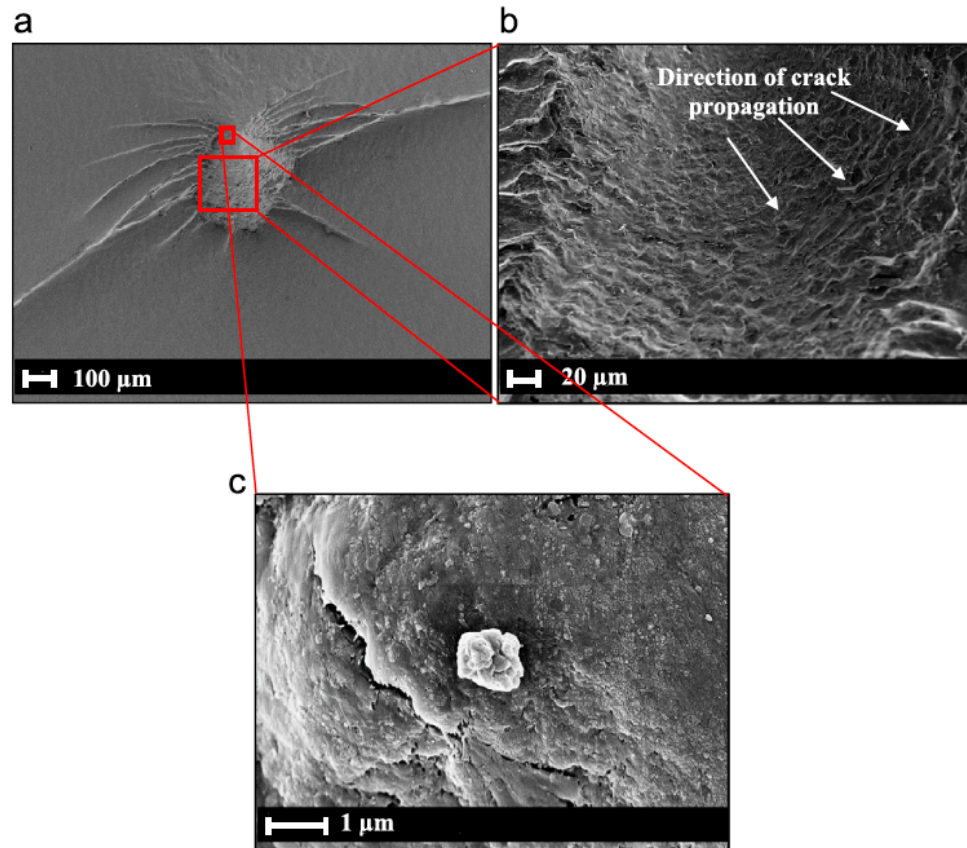


Fig. 7 – (a) Fracture surface of a fatigued specimen at 0.025 mm/mm strain amplitude showing the incubation and crack propagation region, (b) the direction of crack propagation, and (c) incubating particle.

Cracks initiate at micro-inclusions, pores, microcracks; fatigue striations can be identified in stable crack propagation regime

ε -N Fatigue of PEEK

$$N_{\text{total}} = N_{\text{inc}} + N_{\text{MSC/PSC}} + N_{\text{LC}}$$

Where

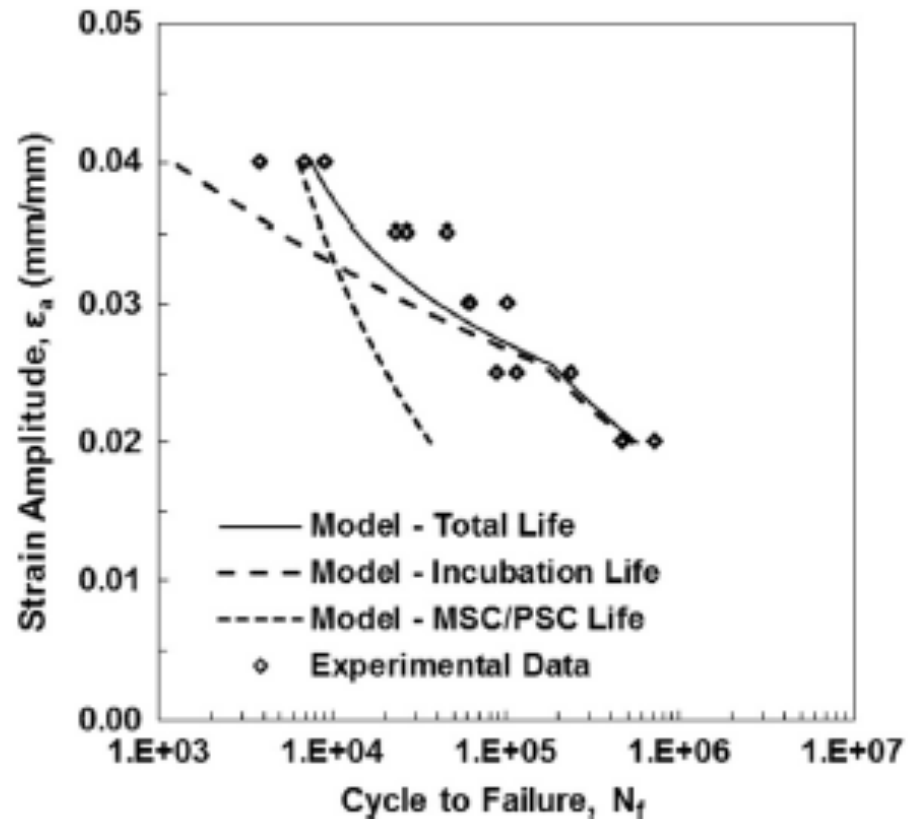
N_{inc} = cycles to incubate a crack

N_{MSC} = cycles, propagation of a microstructurally small crack

N_{PSC} = cycles, propagation of a physically small crack

N_{LC} = cycles for long crack propagation (LEFM regime)

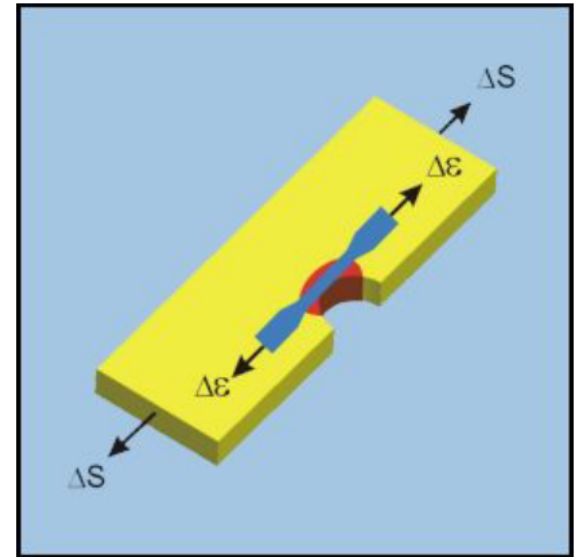
ϵ -N Fatigue of PEEK



Model appears to be predictive of fatigue life – incubation life dominates at low cyclic strains

ϵ -N Fatigue of PEEK - observations

- May be a useful approach to evaluate and predict incubation and initiation of cracks from blunt notches in components where the local conditions are under strain control
- Even low frequency cyclic straining can potentially lead to thermal variations that affect fatigue life; may need to be accounted for unless adiabatic conditions are assured



Fatigue Crack Propagation Behavior of PEEK

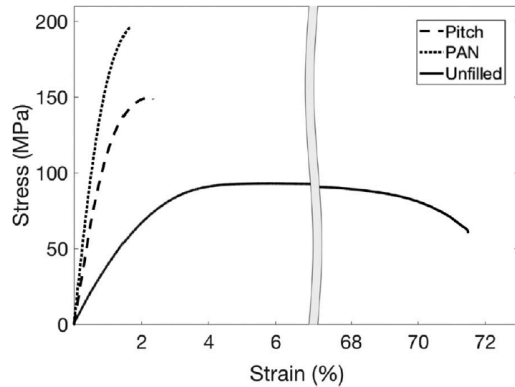
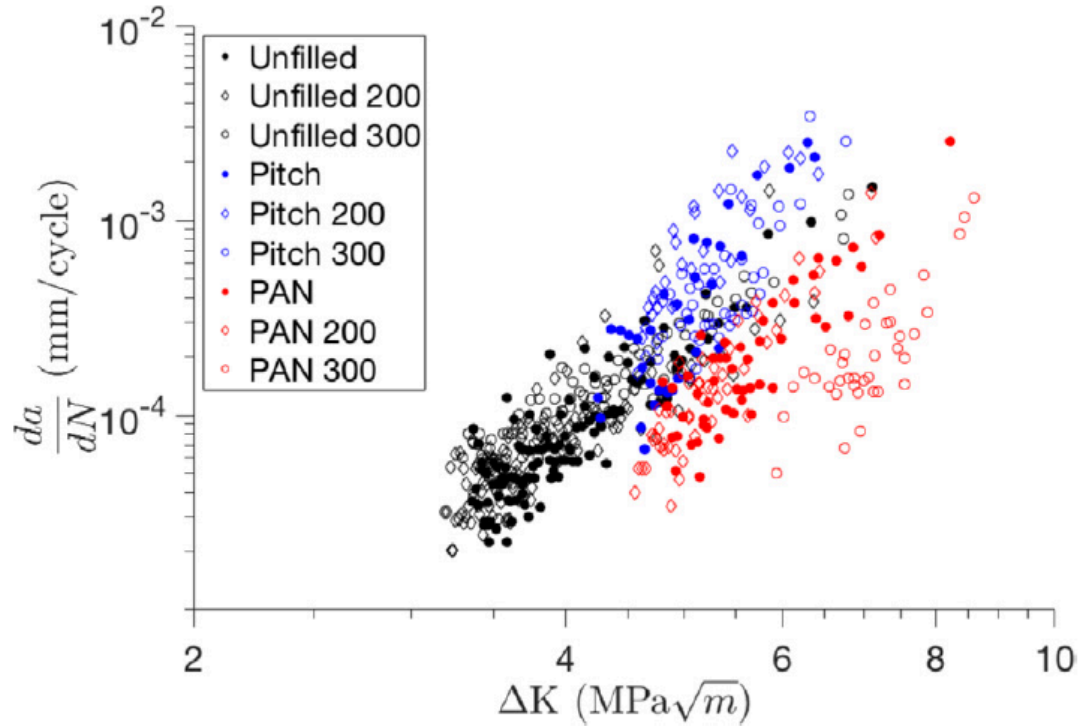
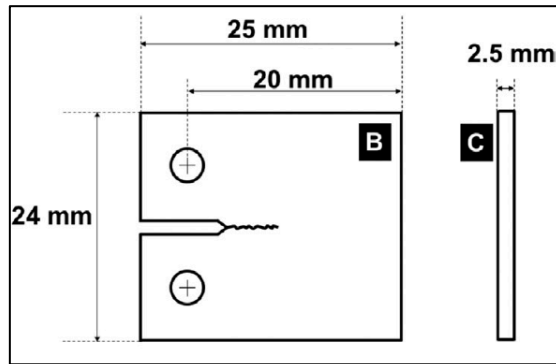
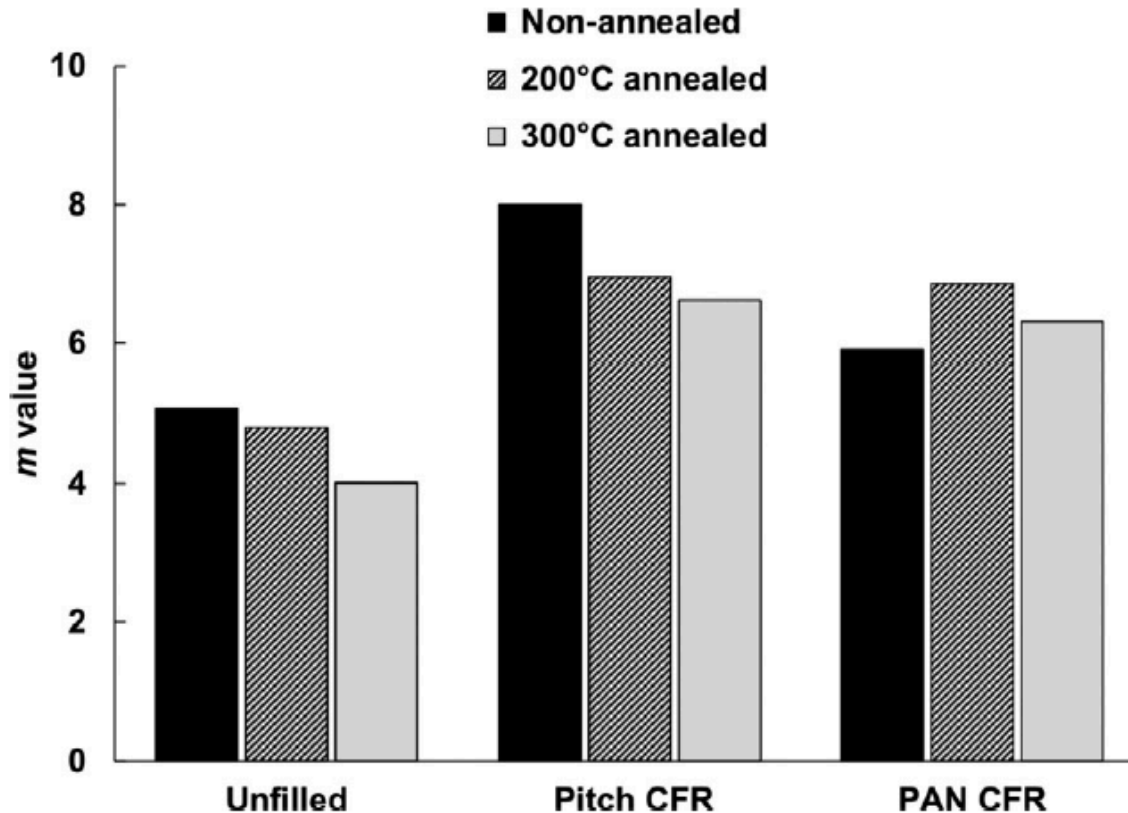


Fig. 2. Representative stress-strain plots for Pitch CFR PEEK, PAN CFR PEEK, and unfilled PEEK (non heat-treated formulations).



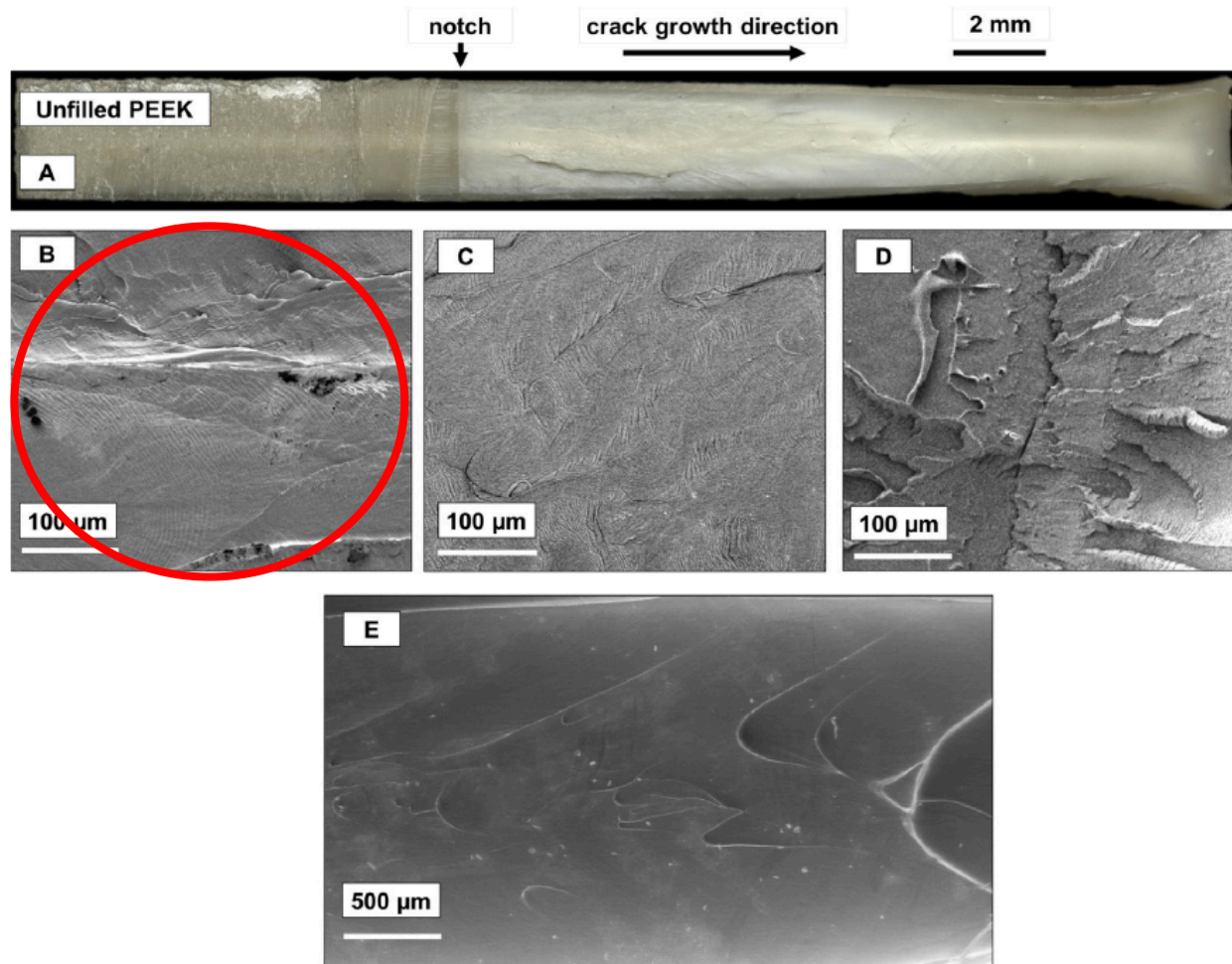
- Carbon fiber reinforcement (PAN) can improve FCP resistance
- PEEK-OPTIMA™ LT1, Invibio; Pitch CFR (PEEK-OPTIMA Wear Performance™); PAN CFR (PEEK-OPTIMA Reinforced™); R= 0.1; RT (air cooled); 5 Hz

Fatigue Crack Propagation Behavior of PEEK



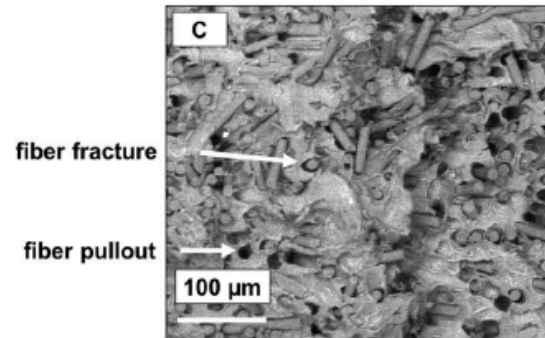
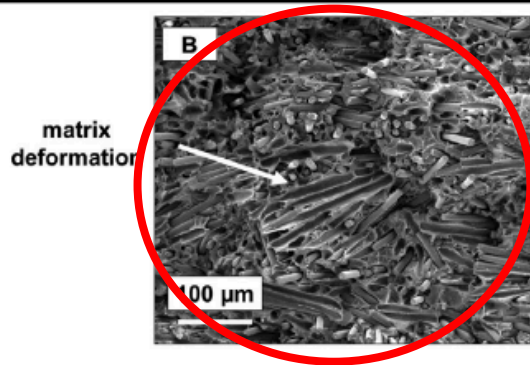
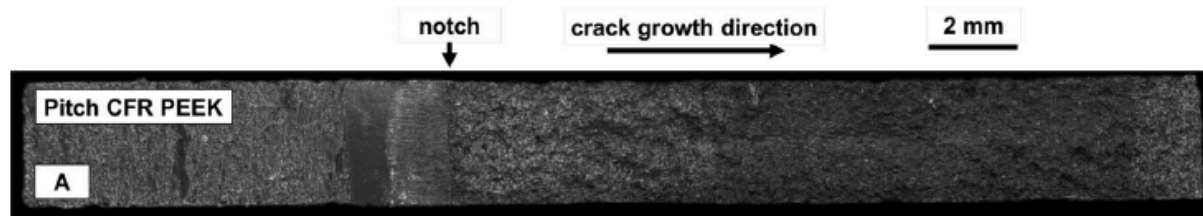
Carbon fiber reinforced increased *m* of Paris relationship versus Unfilled, indicating faster fatigue crack growth

Fracture Appearance

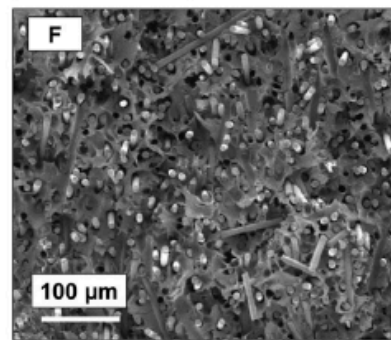
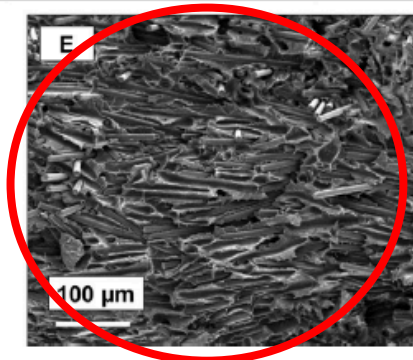
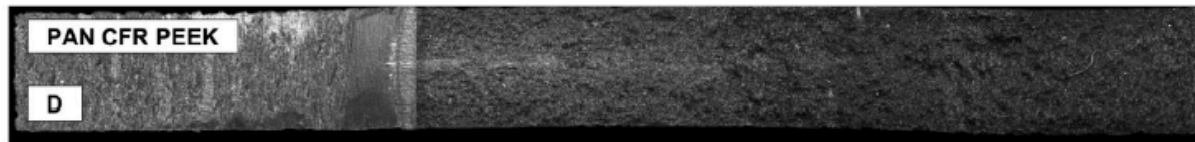


Unfilled PEEK: fatigue striations are evident in stable crack growth regime, transitioning to parabolic markings

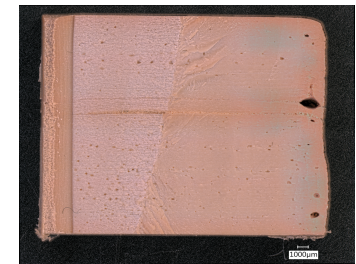
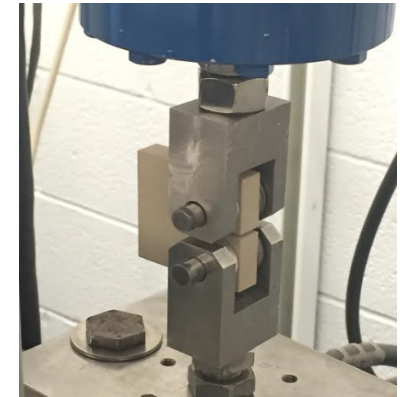
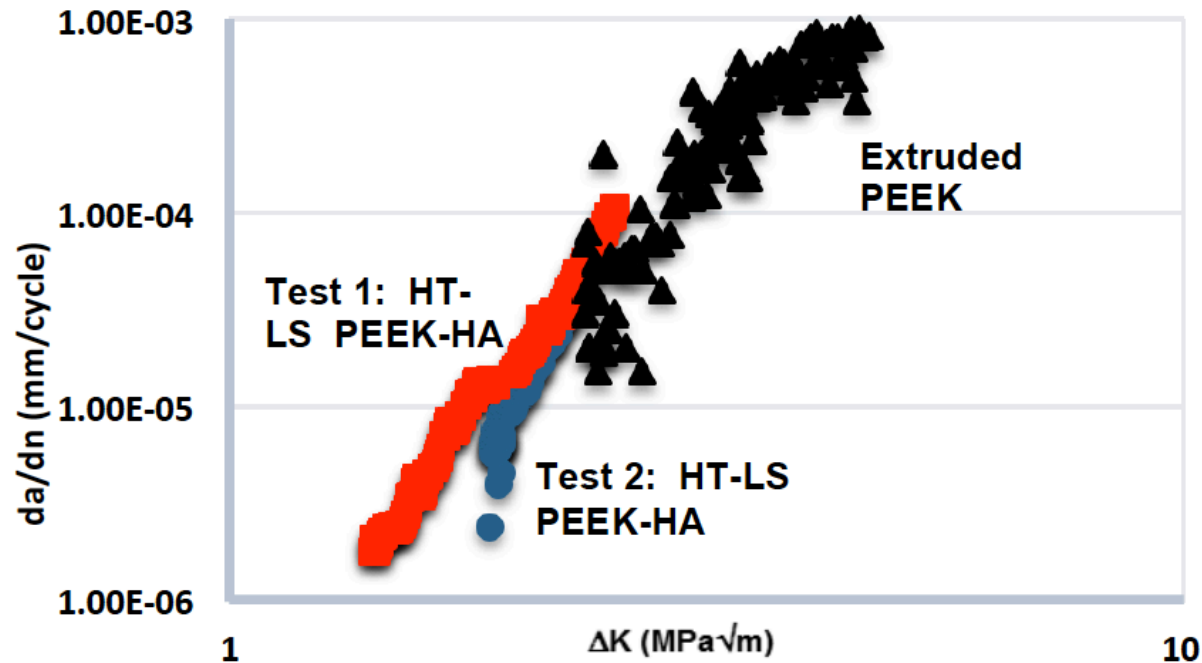
Fracture Appearance



CFR PEEK:
Matrix deformation;
fiber pull-out; fiber
fracture

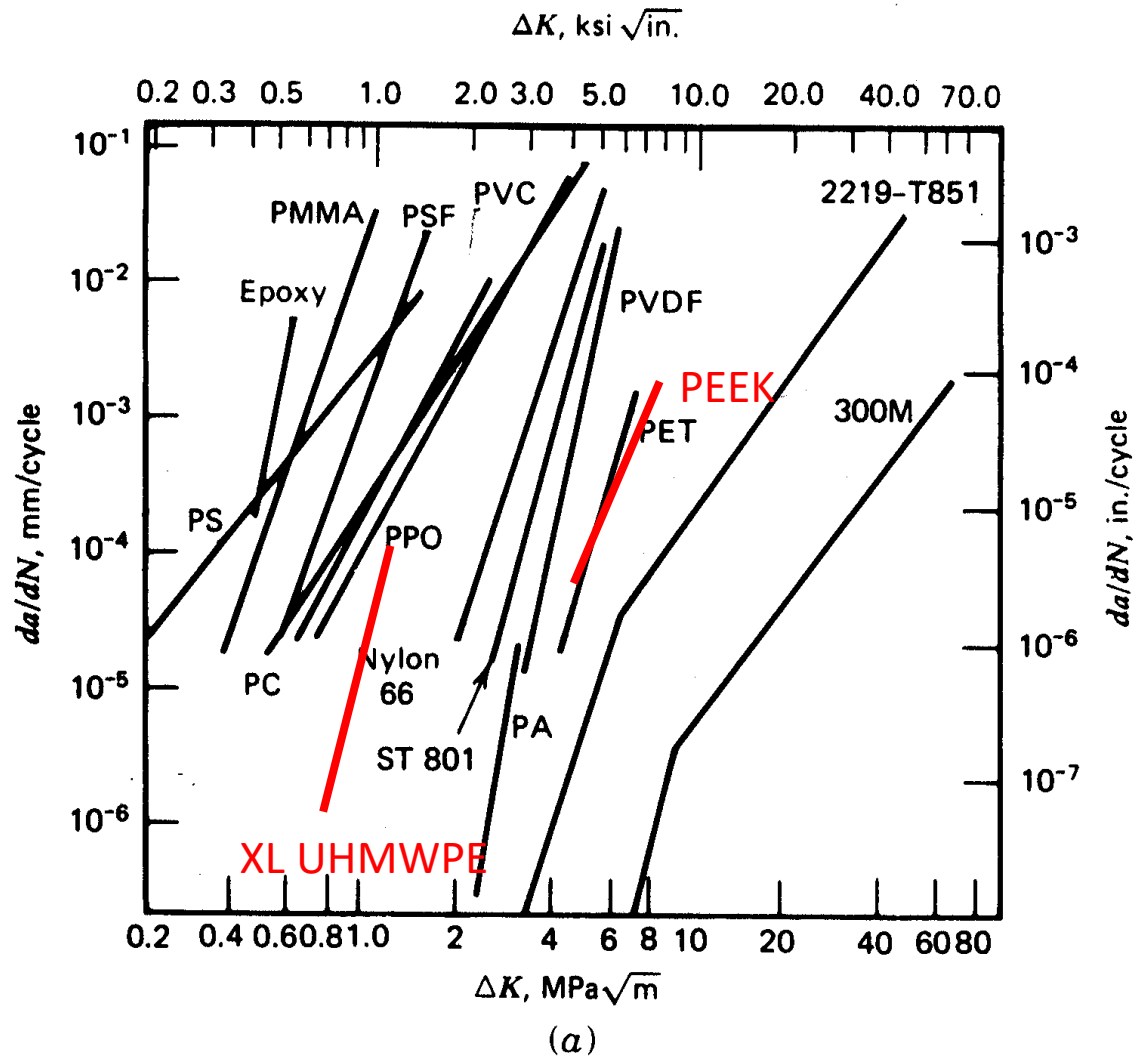


Fatigue Crack Propagation Behavior of PEEK/HA



- HT-LS AM PEEK/HA; $R = 0.1$; RT; 3 Hz
- Achieved stable fatigue crack growth
- Fracture toughness \sim
- PEEK OPTIMA[®] LT1 Invibio, 2% HA; Commercial: Quadrant EPP Ketron 1000

FCP Behavior of PEEK versus Other Materials



Summary/ Directions for Future Studies

- S-N, ϵ -N, and fatigue crack propagation resistance of PEEK is generally high and compares favorably with other structural polymers
- S-N is subject to surface conditions; notching
- ϵ -N is subject to specimen heating arising from cycling
- FCP can be enhanced with CFR (with attention paid to the processing conditions)
- Stable FCP can be achieved in HT-LS PEEK/HA (promising for additively manufactured constructs)

- Still little information on fatigue and fracture performance of medical grade PEEK, particularly for modified and additively manufactured formulations and under physiologically-relevant conditions

Thank you!